



Introduction to radiometric uncertainty **Claire Greenwell**, Emma Woolliams and Agnieszka Bialek 8th May 2017





fiducial reference measurements for satellite ocean colour





Metrology for Earth Observation and Climate http://www.emceoc.org



Programme of EURAMET

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About NPL ...

- Founded in 1900
- World leading National Metrology Institute
- ~750 staff; 550+ specialists in Measurement Science plus 200 visiting researchers pa
- State-of-the-art laboratory facilities
- 388 Laboratories (35,746 sq. metres)
- The heart of the UK's National Measurement System to support business and society
- Experts in Knowledge Transfer





The growing demand for better measurements



2% of GDP dependent on a robust measurement







klogram	kilogram	Mass
m nets	metre	Length
S	second	Time
А	ampere	Electric Current
K ketoka	kelvin	Temperature
cd	candela	Luminous Intensity
mol	mole	Amount of Substance

KC: Luminous intensity





The GUM





The Guide to the expression of Uncertainty in Measurement (GUM)

The foremost authority and guide to the expression and calculation of uncertainty in measurement science Written by the JCGM and BIPM Covers a wide number of applications Technical with formal mathematics

http://www.bipm.org/en/publications/guides/gum.html

First edition September 2008

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Uncertainty – Error – Correction





Traceability



"Property of a measurement result relating the result to a stated metrological reference (free definition and not necessarily SI) through an unbroken chain of calibrations of a measuring system or comparisons, each contributing to the stated measurement uncertainty"

Committee on Earth Observation Satellites (CEOS)

Spectral Radiance and Irradiance







Traceability: further points



Cryogenic radiometer 0.01 %

Primary irradiance standard 0.5 %

Calibration lamp use 'in situ' 1.2 %

Field spectrometer calibration 2.5 %

Vicarious calibration reference 3.2 %

Inverse Square Law of Irradiance



Irradiance Standards



Tungsten-halogen lamp (FEL) 1 kW (~ 3000 K)





Irradiance







Radiance invariance



• Throughput invariance (étendue) $T = A\Omega$



$$A_{s}\Omega_{os} = A_{o}\Omega_{so} = A_{o}\Omega_{do} = A_{d}\Omega_{od} .$$

Assuming lossless beam propagation and no lens transmission

Palmer J.M, 2010

Radiance standards



Lamp –reflectance standard

Integrating sphere





Radiance

Lamp - tile





 $L_{s} = \frac{E_{FEL}\beta_{0:45}}{\pi} \frac{d_{cal}^{2}}{d_{ucc}^{2}}$ use

Reflectance *p***and Reflectance factors**



We have 9 kinds of reflectance and 9 equivalent reflectance factors.

First defined in 1977 by Nicodemous to simply surface scattering phenomena,

Assumptions:

Geometrical ray optics

A flat surface that is uniformly illuminated

Incident radiance depends only on direction

Surface has uniform and isotropic scattering properties

BRDF bidirectional reflectance function

Definition

$$f(\theta_{\mathrm{I}},\varphi_{\mathrm{I}};\theta_{\mathrm{R}},\varphi_{\mathrm{R}},\lambda) = \frac{dL_{\mathrm{R}}(\theta_{\mathrm{I}},\varphi_{\mathrm{I}};\theta_{\mathrm{R}},\varphi_{\mathrm{R}},\lambda,E_{I})}{dE_{\mathrm{I}}(\theta_{\mathrm{I}},\varphi_{\mathrm{I}})}$$



Measurement equation

BRDF=

$$f_r(\theta_{\mathrm{I}},\varphi_{\mathrm{I}},\theta_{\mathrm{R}},\varphi_{\mathrm{R}},\lambda) = d\rho(\theta_{\mathrm{I}},\varphi_{\mathrm{I}},\theta_{\mathrm{R}},\varphi_{\mathrm{R}},\lambda) = \lim_{\Omega \to 0} \frac{\Phi_{\mathrm{R}}(\theta_{\mathrm{I}},\varphi_{\mathrm{I}},\theta_{\mathrm{R}},\varphi_{\mathrm{R}},\lambda)}{\Phi_{\mathrm{I}}(\lambda)\cos\theta_{\mathrm{R}}\Omega}$$





BRF bidirectional reflectance factor

$$BRF\left(\theta_{i};\theta_{r},\lambda\right) = BRDF \cdot \pi = \lim_{\Omega \to 0} \frac{\Phi_{R}(\theta_{I},\theta_{R},\lambda)}{\Phi_{I}(\lambda)\cos\theta_{R}\Omega} \cdot \pi$$

the ratio of the radiance flux actually reflected by a sample surface to that which would be reflected into the same reflected-beam geometry by an ideal perfectly diffuse standard surface irradiated in exactly the same way as the sample

Radiometers



Multispectral

Stable and reliable Limited spectral information



Ehsani et al. 1998



Hyperspectral

Demanding characterisation necessary ! "Full" spectral information





Steps to an uncertainty budget

NATIONAL Physical Laboratory

- 1. Traceability Chain
- 2. Calculation Equation
- 3. Sources of Uncertainty
- 4. Measurement Equation
- 5. Sensitivity Coefficients
- 6. Assigning Uncertainties
- 7. Combining your uncertainties

Symbol	Uncertainty component	Size of effect	Correction applied?	Residual uncertainty	Divisor	Sensitivity coefficient	Uncertainty associated with final value due to effect
Combined standard uncertainty							
Expanded uncertainty							

Step 1: Traceability chain





Step 2: Calculation equations





Step 3: Sources of uncertainty





Lamp

Lamp additional effects

- Ageing
- Alignment
- Current stability



Diffuser

Diffuser additional effects

- Ageing
- Uniformity



Distance accuracy



Random noise

Instrument additional effects

- Stability (drift)
- Room stray light

Step 4: Measurement equations





$$V_{\rm S} = V_{\rm light} - V_{\rm dark}$$
$$V_{\rm S} = V_{\rm light} K_{\rm light_stab} + K_{\rm stray} - V_{\rm dark} K_{\rm dark_stab}$$



Determining the sensitivity coefficients

• Do an experiment

Analytical expression

• Model it





 $y'_{n} g = n^{2} + 3\sqrt{n} - \Lambda \quad n = x^{4} + \Lambda g'_{x} = \frac{1}{2}$ $= (n^{2} + 3\sqrt{n} - \Lambda)_{n} (x^{4} + \Lambda)'_{x} = (2n^{4} + n)^{2}$ $= (2n^{4} + 3\sqrt{n} - \Lambda)_{n} (x^{4} + \Lambda)'_{x} = (2n^{4} + n)^{2}$ $= (2n^{4} + 2 + 2n^{2})^{2} + (1 + 2n^{2})^{2}$ $= (1 + \frac{2}{x})^{x+5} = ((1 + \frac{2}{x})^{\frac{x}{2}})^{2} + (1 + \frac{2}{x})^{5} / i_{n}$ $= (1 + \frac{2}{x})^{x+5} = ((1 + \frac{2}{x})^{\frac{x}{2}})^{2} + (1 + \frac{2}{x})^{5} / i_{n}$ $= (1 + \frac{2}{x})^{x+5} = ((1 + \frac{2}{x})^{\frac{x}{2}})^{2} + (1 + \frac{2}{x})^{5} / i_{n}$ $= (1 + \frac{2}{x})^{x+5} = ((1 + \frac{2}{x})^{\frac{x}{2}})^{2} + (1 + \frac{2}{x})^{5} / i_{n}$ $= (1 + \frac{2}{x})^{x+5} = (1 + \frac{2}{x})^{\frac{x}{2}} + (1 + \frac{2}{x})^{5} / i_{n}$ $= (1 + \frac{2}{x})^{x+5} = (1 + \frac{2}{x})^{\frac{x}{2}} + (1 + \frac{2}{x})^{5} / i_{n}$ $= (1 + \frac{2}{x})^{x+5} = (1 + \frac{2}{x})^{\frac{x}{2}} + (1 + \frac{2}{x})^{5} / i_{n}$ $= (1 + \frac{2}{x})^{x+5} = (1 + \frac{2}{x})^{\frac{x}{2}} + (1 + \frac{2}{x})^{5} / i_{n}$ $= (1 + \frac{2}{x})^{x+5} = (1 + \frac{2}{x})^{\frac{x}{2}} + (1 + \frac{2}{x})^{5} / i_{n}$ $= (1 + \frac{2}{x})^{x+5} = (1 + \frac{2}{x})^{\frac{x}{2}} + (1 + \frac{2}{x}$

Uncertainties of calculation calibration NPL equation components (1) certificates

Component x_i	Sensitivity coefficient $c_i = \frac{\partial f}{\partial x_i}$	Relative radiance uncertainty due to $c_i u(x_i)$
Lamp irradiance E_{FEL}	$L_{ m s}/E_{ m FEL}$	$1 \cdot u(E_{\text{FEL}})/E_{\text{FEL}}$
Radiance factor $\beta_{0:45}$	$L_{ m s}/eta_{ m 0:45}$	$1 \cdot u(\beta_{0:45}) / \beta_{0:45}$
Distance d_{use}^2	$-2L_{\rm s}/d_{\rm use}$	$-2 \cdot u(d_{\rm use})/d_{\rm use}$
$\left(\frac{u(L)}{L}\right)^2$	$^{2} = \left(\frac{u(E_{\text{FEL}})}{E_{\text{FEL}}}\right)^{2} + \left(\frac{u(\beta_{0:45})}{\beta_{0:45}}\right)^{2}$	$\Big)^{2} + \left(-2\right)^{2} \left(\frac{u(d_{\text{use}})}{d_{\text{use}}}\right)^{2}$

Certificate uncertainties





640

7.68

Certificate may not give required quantity (modelling may be needed to obtain desired quantity): read it carefully! 5.96 590 1.4 1.4 595 6.14 1.3 6.31 600 605 6.48 Integration and/or interpolation 610 6.65 615 6.83 may need to be done if the 620 7.00 625 7.18 wavelength values or radiometer 630 7.35 635 7.52 bands do not match

Uncertainties of calculation equation components - sensitivity



Component x_i	Sensitivity coefficient $c_i = \frac{\partial f}{\partial x_i}$	Relative radiance uncertainty due to $c_i \mu(x_i)$
Lamp irradiance E _{FEL}	$L_{ m s}/E_{ m FEL}$	$1 \cdot u(E_{\text{FEL}})/E_{\text{FEL}}$
Radiance factor $\beta_{0:45}$	$L_{ m s}/eta_{ m 0:45}$	$1 \cdot u(\beta_{0:45}) / \beta_{0:45}$
Distance d_{use}^2	$-2L_{\rm s}/d_{\rm use}$	$-2 \cdot u(d_{use})/d_{use}$
$\left(\frac{u(L)}{L}\right)^2$	$^{2} = \left(\frac{u\left(E_{\text{FEL}}\right)}{E_{\text{FEL}}}\right)^{2} + \left(\frac{u\left(\beta_{0:45}\right)}{\beta_{0:45}}\right)^{2}$	$\bigg)^{2} + \left(-2\right)^{2} \left(\frac{u(d_{\text{use}})}{d_{\text{use}}}\right)^{2}$

Rectangular uncertainty distributions Resolution of distance measuring instrument = 0.1 mm

 $-2 \cdot u(d_{use})/d_{use}$

Measurement distance = 500.0 mm

Uncertainty associated with distance measurement = $(0.05 / 500) / \sqrt{3} = 0.006 \%$

Uncertainty in irradiance from distance measurement = $2 \times 0.006 \% = 0.012 \%$





Uncertainties of calculation equation components $\left(\frac{u(L)}{L}\right)^{2} = \left(\frac{u(E_{\text{FEL}})}{E_{\text{EFI}}}\right)^{2} + \left(\frac{u(\beta_{0:45})}{\beta_{0:45}}\right)^{2} + \left(-2\right)^{2} \left(\frac{u(d_{\text{use}})}{d_{\text{use}}}\right)^{2}$



Symbol	Uncertainty component	Size of effect	Correction applied?	Residual uncertainty	Divisor	Sensitivity coefficient	Uncertainty associated with final value due to effect
$u(E_{\rm FEL})$	Ref. lamp irradiance	1.5 %	N	1.5 %	2	1	0.75 %
$u(\beta_{0:45})$	Tile radiance factor	2.0 %	N	2.0 %	2	1	1.00 %
$u(d_{use})$	Lamp distance (500 mm)	0.05 mm	N	0.01 %	√3	2	0.012 %
$u(d_{use})$							
$u(d_{use})$							
$u(d_{use})$							
$u(d_{use})$							
$u(d_{use})$							
$u(d_{use})$							
$u(d_{use})$							
$u(d_{use})$							
Combined standard uncertainty							
Expanded uncertainty							

Uncertainty of additional effects NPL (1)





Repeat measurements with realignment of the lamp

Uncertainty of additional effects (2)



Negligible instrument drift
 in controlled lab environment
 0.7 DN change during
 45 minute constant run



 $V_{\rm S} = V_{\rm light}$ $K_{\rm stab} + K_{\rm stray} - V_{\rm dark}$

Uncertainty of additional effects NPL (3)



$$V_{\rm S} = V_{\rm light} K_{\rm light_stab} + K_{\rm stray} - V_{\rm dark} K_{\rm dark_stab}$$

Uncertainty of additional effects NPL (4)



Uncertainty of additional effects (5)



Difference between detector dark reading and measurement with detector FOV obscured smaller than standard deviation of individual dark runs

Room stray light negligible



 $V_{\rm S} = V_{\rm light} K_{\rm light_stab} + K_{\rm stray} - V_{\rm dark} K_{\rm dark\ stab}$

Uncertainty of additional effects **NPL** (6)

$$L_{\rm s} = \frac{E_{\rm FEL}\beta_{0:45}}{\pi} \frac{d_{\rm cal}^2}{d_{\rm use}^2} K_{\rm lamp_stab} K_{\rm align} K_{\rm current} K_{\rm diff_stab} K_{\rm unif}$$

By modelling (or by measurement)

$$V_{\rm S} = V_{\rm light} K_{\rm light_stab} + K_{\rm stray} - V_{\rm dark} K_{\rm dark_stab}$$

Uncertainty of additional effects (7)

Relationship between lamp current and irradiance **modelled** by:



reat current uncertainty as rectangular distribution

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Lamp current effect by measurement



Suppose:

Lamp current uncertainty is 0.020 A Lamp current is 8.000 A Lamp CCT is 3000 K

• We can **measure** the effect by:

Measuring irradiance at a current of 8.000 A Measuring irradiance at a current of (say) 7.800 A (needs to be large enough difference to enable effect to be measured reliably)

 $u(E_{current}) = 0.1 \text{ x observed relative change in irradiance due to 0.200 A change in current}$

Uncertainty of additional effects NPL (8)



$$V_{\rm S} = V_{\rm light} K_{\rm light_stab} + K_{\rm stray} - V_{\rm dark} K_{\rm dark_stab}$$

Uncertainty of additional effects (9)

Measured uniformity and consideration of where radiometer is placed



Worst case uncertainty is ± 1.5 %

Even if diffuser is perfectly uniform, non-uniformity due to lamp irradiance can be large, especially at short distances (inverse square law)



Combined uncertainty



Symbol	Uncertainty component	Size of effect	Correction applied?	Residual uncertainty	Divisor	Sensitivity coefficient	Uncertainty associated with final value due to effect
$u(E_{\rm FEL})$	Ref. lamp irradiance	1.5 %	N	1.5 %	2	1	0.75 %
$u(\beta_{0:45})$	Tile radiance factor	2.0 %	N	2.0 %	2	1	1.00 %
$u(d_{use})$	Lamp distance (500 mm)	0.05 mm	N	0.01 %	√3	2	0.012 %
$u(K_{align})$	Lamp alignment	0.15 %	N	0.15 %	1	1	0.15 %
$u(K_{l_{stab}})$	Light reading stability	negligible	N	negligible			negligible
$u(K_{d_{stab}})$	Dark reading stability	negligible	N	negligible			negligible
$u(K_{lamp_{stab}})$	Lamp stability	0.083 %	N	0.083 %	√3	1	0.048 %
$u(K_{diff_{stab}})$	Diffuser stability	0.125 %	N	0.125 %	√3	1	0.072 %
$u(K_{\text{stray}})$	Stray light in lab	negligible	N	negligible			negligible
u(K _{current})	Lamp current (8.000 A)	0.004 A	N	0.25 % in <i>I</i> , or 0.99 % in <i>E_{FEL}</i> at 600 nm	√3	1	0.572 % (at 600 nm)
$u(K_{\text{unif}})$	Radiance uniformity	1.50 %	N	1.50 %	√3	1	0.866 %
Combined standard uncertainty							1.63 %
Expanded uncertainty (<i>k</i> =2)						3.3 %	

Expanding uncertainties





If the distribution is not Gaussian, then a different coverage factor is needed.

Conclusions



1. Traceability Chain

Show linkage back to 'point of trust'

2. Calculation Equation

Equation for each step in measurement process / step in chain

3. Sources of Uncertainty

Consider all factors that may affect result for each calculation equation

4. Measurement Equation

Include all sources of uncertainty

Types of uncertainty (multiplicative, additive)

Conclusions



5. Sensitivity Coefficients

Mathematically, from experimental investigations, or by modelling

6. Assigning Uncertainties

Other information (e.g. certificates, historical data, other researchers), statistical analysis, experimental studies, modelling, or combination

- Combining your uncertainties
 When to stop
- 8. Expanding your uncertainties





- SI traceability ensures the valid measurements
- Calibration links instrument output readings to physical values
- SI traceability especially important to radiometry, as these measurements are used calibration and validation of satellite sensors
- Instrument characteristics influence their properties and performance







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